AOE 3134 Stability and Control Important Equations and Relations

March 12, 2002

1. Longitudinal Static Stability

a. General

i. General moment relation between two reference points

$$C_{m_{(b)}} = C_{m_{(a)}} + C_L (h_b - h_a)$$

ii. Aerodynamic center: $C_{m_{AC}}$ = constant independent of angle-of-attack $C_{m_{AC}}$ = $C_{m_{0L}}$

$$C_{m_{(x)}} = C_{m_{0L}} + C_L(h_{(x)} - h_{ac}) = C_{m_{0L}} + C_L(h_{(x)} - h_n)$$

b. Lift related characteristics

i. Lift curve slope of aircraft $C_{L_n} = a$

$$C_{L_{\alpha}} = a = a_{wb} \left[1 + \frac{a_{ht}}{a_{wb}} \eta_{ht} \frac{S_{ht}}{S} \left(1 - \frac{\partial \epsilon}{\partial \alpha} \right) \right]$$

ii. Lift coefficient at zero angle-of-attack C_{L_0}

(Note: usually $i_w = 0$, it is not zero if the wing is treated separately from the fuselage, then $a_{wb} = a_w$, etc.)

$$C_{L_0} = a_{wb} \left\{ \left(i_w - \alpha_{0L_{wb}} \right) + \frac{a_{ht}}{a_{wb}} \eta_{ht} \frac{S_{ht}}{S} \left[i_{ht} - \epsilon_{0_{wb}} - \alpha_{0L_{ht}} - \frac{\partial \epsilon}{\partial \alpha} \left(i_w - \alpha_{0L_{wb}} \right) \right] \right\}$$

iii. Aircraft zero-lift angle of attack, α_{oL}

$$\alpha_{0L} = -\frac{C_{L_0}}{a}$$

iv. Elevator control deflection contribution to lift, $C_{L_{\delta_e}}$

$$C_{L_{\delta_e}} = a_e \eta_{ht} \frac{S_{ht}}{S} = a_{ht} \tau_e \eta_{ht} \frac{S_{ht}}{S}$$

Note: For full "flying tail" τ_{e} = 1, and δ_{e} = Δi_{ht}

v. Total tail lift coefficient

$$C_{L_{ht}} = a_{ht} \overline{\alpha}_{ht} + a_e \delta_e$$

vi. Aircraft lift characteristics

$$C_{L} = C_{L_{\alpha}} (\alpha - \alpha_{0L}) + C_{L_{\delta_{e}}} \delta_{e}$$

$$C_{L} = C_{L_{\alpha}} \overline{\alpha} + C_{L_{\delta_{e}}} \delta_{e} = a \overline{\alpha} + C_{L_{\delta_{e}}} \delta_{e}$$

$$C_{L} = C_{L_{0}} + C_{L_{\alpha}} \alpha + C_{L_{\delta_{e}}} \delta_{e}$$

Also

$$C_L = C_{L_{wb}} + C_{L_{ht}} \eta_{ht} \frac{S_{ht}}{S}$$

- c. Moment related characteristics
 - i. Aircraft moment

$$C_{m} = C_{m_{0L_{wb}}} + C_{L_{wb}}(h - h_{n_{wb}}) - \eta_{ht} V_{ht} C_{L_{ht}}$$
$$C_{m} = C_{m_{0L_{w}}} + C_{L_{w}}(h - h_{n_{w}}) - \eta_{ht} V_{ht} C_{L_{ht}} + C_{m_{fn}}$$

where

$$V_{ht} = \frac{S_{ht}}{S} \frac{l_{ht}}{\overline{c}} = \frac{S_{ht}}{S} \cdot (h_{ht} - h)$$
$$l_{ht} = (h_{ht} - h) \cdot \overline{c} = \text{tail length}$$

$$\overline{l}_{ht} = (h_{ht} - h_{n_{wb}}) \overline{c} \doteq \text{modified tail length}$$

ii. Aircraft longitudinal stability parameter

$$C_{m_{\alpha}} = a_{wb} \left[(h - h_{n_{wb}}) - \frac{a_{ht}}{a_{wb}} \eta_{ht} V_{ht} \left(1 - \frac{\partial \epsilon}{\partial \alpha} \right) \right]$$
$$C_{m_{\alpha}} = a_{w} \left[(h - h_{n_{w}}) - \frac{a_{ht}}{a_{w}} \eta_{ht} V_{ht} \left(1 - \frac{\partial \epsilon}{\partial \alpha} \right) \right] + \frac{\partial C_{m}}{\partial \alpha} \right]_{fn}$$

The wing-fuselage aerodynamic center location is related to the wing aerodynamic center location by the following approximate relationship:

$$h_{n_{wb}} = h_{n_w} - \frac{1}{a_w} \frac{\partial C_m}{\partial \alpha} \bigg|_{fn}$$

iii. Aircraft zero lift moment

$$C_{m_{0L}} = C_{m_{0L_{wb}}} + a_{ht} \eta_{ht} \frac{S_{ht}}{S} (h_{ht} - h_{n_{wb}}) \frac{a_{wb}}{a} (i_w - \alpha_{0L_{wb}} - i_{ht} + \epsilon_{0L_{wb}} + \alpha_{0L_{ht}})$$

iv. Aircraft pitch control power

$$C_{m_{\delta_e}} = -a_e \eta_{ht} V_{ht}$$

v. Aircraft pitch-moment equation

$$C_m = C_{m_{0L}} + C_{m_{\alpha}} \overline{\alpha} + C_{m_{\delta_e}} \delta_e$$
$$C_m = C_{m_0} + C_{m_{\alpha}} \alpha + C_{m_{\delta_e}} \delta_e$$

d. Stick fixed stability parameters

i. Stick fixed neutral point (Aircraft aerodynamic center)

$$C_{m_{\alpha}} = a(h - h_n)$$

also

where

$$h_{n} = \frac{h_{n_{wb}} + \frac{a_{ht}}{a_{wb}} \eta_{ht} \frac{S_{ht}}{S} h_{ht} \left(1 - \frac{\partial \epsilon}{\partial \alpha}\right)}{1 + \frac{a_{ht}}{a_{wb}} \eta_{ht} \frac{S_{ht}}{S} \left(1 - \frac{\partial \epsilon}{\partial \alpha}\right)}$$
$$h_{n} = h_{n_{wb}} + \frac{a_{ht}}{a} \eta_{ht} \frac{S_{ht}}{S} (h_{ht} - h_{n_{wb}}) \left(1 - \frac{\partial \epsilon}{\partial \alpha}\right)$$

ii. Stick fixed static margin

$$K_n \doteq h_n - h$$

iii. Maximum forward cg position (from balanced-level-flight-control point of view)

$$h_{\min} = h_n - \frac{\Delta}{a C_{L_{\max}}} \left[\frac{C_{m_{0L}} C_{L_{\alpha}}}{\Delta} - |\delta_e|_{\max} \right]$$

- 2. Aircraft equilibrium (balanced flight) equations
 - a. Balanced flight equations

$$C_{L} = C_{L_{\alpha}} \overline{\alpha} + C_{L_{\delta_{e}}} \delta_{e} = \frac{L}{1/2 \rho V^{2} S}$$
$$C_{m} = C_{m_{0L}} + C_{m_{\alpha}} \overline{\alpha} + C_{m_{\delta_{e}}} \delta_{e} = 0$$

b. Elevator angle and angle of attack for balanced flight

$$\overline{\alpha} = \frac{C_{L_{\delta_e}}C_{m_{0L}} + C_{m_{\delta_e}}C_L}{\Delta}$$
$$\delta_e = -\left[\frac{C_{L_{\alpha}}C_{m_{0L}} + C_{m_{\alpha}}C_L}{\Delta}\right]$$

where

$$\Delta = C_{L_{\alpha}} C_{m_{\delta_e}} - C_{m_{\alpha}} C_{L_{\delta_e}}$$

3. Longitudinal control surface considerations

a. Elevator hinge moment

$$C_{H_e} = \frac{H_e}{\frac{1}{2} \rho V_{ht}^2 S_e \overline{c}_e}$$

= $C_{h_{e_0}} + \frac{\partial C_{H_e}}{\partial \alpha_{ht}} \overline{\alpha}_{ht} + \frac{\partial C_{H_e}}{\partial \delta_e} \delta_e + \frac{\partial C_{H_e}}{\partial \delta_t} \delta_t$
= $b_0 + b_1 \overline{\alpha}_{ht} + b_2 \delta_e + b_3 \delta_t$

b. Stick free, $C_{H_e} = 0$ (assume $b_0 = 0$ and $\delta_t = 0$, for convenience only)

i. Elevator float angle

$$\delta_e = -\frac{b_1}{b_2} \alpha_{ht}$$

c. Stick free properties - replace a_{ht} with $\hat{a}_{ht} = F a_{ht}$

where
$$F = 1 - \frac{a_e}{a_{ht}} \frac{b_1}{b_2}$$
 = the free elevator factor

i. Lift-curve slope

$$\hat{a} = a_{wb} \left[1 + F \frac{a_{ht}}{a_{wb}} \eta_{ht} \frac{S_{ht}}{S} \left(1 - \frac{\partial \epsilon}{\partial \alpha} \right) \right]$$

ii. Longitudinal stability parameter

$$\hat{C}_{m_{\alpha}} = a_{wb} \left[h - h_{n_{wb}} - F \frac{a_{ht}}{a_{wb}} \eta_{ht} V_{ht} \left(1 - \frac{\partial \epsilon}{\partial \alpha} \right) \right]$$

iii. Stick free neutral point

$$\hat{h}_{n} = \frac{h_{n_{wb}} + F \frac{a_{ht}}{a_{wb}} \eta_{ht} \frac{S_{ht}}{S} h_{ht} \left(1 - \frac{\partial \epsilon}{\partial \alpha}\right)}{1 + F \frac{a_{ht}}{a_{wb}} \eta_{ht} \frac{S_{ht}}{S} \left(1 - \frac{\partial \epsilon}{\partial \alpha}\right)}$$
$$\hat{h}_{n} = h_{n_{wb}} + F \frac{a_{ht}}{\hat{a}} \eta_{ht} \frac{S_{ht}}{S} (h_{ht} - h_{n_{wb}}) \left(1 - \frac{\partial \epsilon}{\partial \alpha}\right)$$

- 4. Stick force characteristics
 - a. Stick force general

$$F_s = G C_{H_e} \eta_{ht} \frac{1}{2} \rho V^2 S_e \overline{c}_e$$

b. Stick force at off-trimmed conditions

$$F_{s} = G \eta_{ht} S_{e} \overline{c}_{e} \frac{W}{S} \frac{b_{2}}{\Delta} \hat{a} (h - \hat{h}_{n}) \left(\frac{V^{2}}{V_{trim}^{2}} - 1 \right)$$

c. stick-force gradient

$$\frac{dF_s}{dV}\bigg|_{V_{trim}} = 2G\eta_{ht}S_e\overline{c}_e\frac{W}{S}\frac{b_2}{\Delta}\hat{a}\frac{(h-\hat{h}_n)}{V_{trim}}$$

5. Maneuvering Flight

a. Pitch damping stability derivatives

$$C_{m_q} = \frac{\partial C_m}{\partial \left(\frac{q \, \overline{c}}{2 \, V}\right)} = -2 \, K \, a_{ht} \sqrt{(\eta_{ht})} \, V_{ht} \frac{l_{ht}}{\overline{c}}$$

where K = 1.1

$$C_{L_q} = \frac{\partial C_L}{\partial \left(\frac{q \, \overline{c}}{2 \, V}\right)} = 2 \, a_{ht} \sqrt{\eta_{ht}} \, V_{ht}$$

b. Elevator angle requirements, (Fac) = 1 for pull-up, = (n+1)/n for horizontal turn

i. Elevator increment for maneuver

$$\Delta \delta_{e} = -\frac{(n-1)C_{w}\left[C_{m_{\alpha}} + (C_{L_{\alpha}}C_{m_{q}} - C_{m_{\alpha}}C_{L_{q}})(Fac)\frac{\rho S \overline{c}}{4m}\right]}{\Delta}$$

ii. Elevator angle / g

$$\frac{\partial \Delta \delta_{e}}{\partial n} = -\frac{C_{w} \left[C_{m_{\alpha}} + (C_{L_{\alpha}} C_{m_{q}} - C_{m_{\alpha}} C_{L_{q}}) (Fac) \frac{\rho S \overline{c}}{4 m} \right]}{\Delta}$$
$$= -\frac{C_{w} C_{L_{\alpha}} \left(\frac{4 m}{\rho S \overline{c}} - C_{L_{q}} \right)}{\frac{4 m}{\rho S \overline{c}} \Delta} (h - h_{mp}) \quad (\text{pull up})$$

iii. Stick fixed maneuver point

$$h_{mp} = h_n - \frac{C_{m_q}}{\left(\frac{4 m}{\rho S \overline{c}}\right) - C_{L_q}}$$

iv. Stick force / g

$$\frac{\partial (\Delta F_s)}{\partial n} = -G \eta_{ht} S_e \overline{c}_e \frac{W}{S} \hat{a} b_2 \frac{\left(\frac{4m}{\rho S \overline{c}} - C_{L_q}\right)}{\frac{4m}{\rho S \overline{c}} \Delta} (h - \hat{h}_{mp})$$

where the stick free maneuver point \hat{h}_{mp} is given by

$$\hat{h}_{mp} = h_{mp} + \frac{\Delta}{\hat{a} b_2} \left[\frac{b_1 \left(1 - \frac{\partial \epsilon}{\partial \alpha} \right)}{a} + \frac{2 b_1 (h_{ht} - h)}{\sqrt{\eta_{ht}} \left(\frac{4 m}{\rho S \overline{c}} - C_{L_q} \right)} \right]$$

Note: b_1 in the third term on the right must be in units of /rad! 7. Lateral directional characteristics

a. Yawing moment

i. Aircraft yaw moment

$$C_{n} = C_{n_{wb}} - \eta_{vt} V_{vt} C_{L_{vt}}$$
$$= C_{n_{wb}} - \eta_{vt} V_{vt} [a_{vt} (\sigma - \beta) + a_{r} \delta_{r}]$$
$$= C_{n_{\beta}} \beta + C_{n_{\delta_{r}}} \delta_{r}$$

ii. Directional stability parameter $C_{n_{\beta}}$

$$C_{n_{\beta}} = \frac{\partial C_{n}}{\partial \beta} = C_{n_{\beta}}\Big|_{wb} + a_{vt} \eta_{vt} V_{vt} \left(1 - \frac{\partial \sigma}{\partial \beta}\right) > 0 \quad \text{for stability}$$

iii. Directional (rudder) control power

$$C_{n_{\delta_r}} = \frac{\partial C_n}{\partial \delta_r} = -a_r \eta_{vt} V_{vt} = -a_{vt} \tau_r \eta_{vt} V_{vt}$$

iv. Stick free stability parameter

$$\hat{C}_{n_{\beta}} = C_{n_{\beta}}\Big|_{wb} + F_{r} a_{vt} \eta_{vt} V_{vt} \left(1 - \frac{\partial \sigma}{\partial \alpha} \right)$$

where

$$F_r = 1 - \frac{a_r}{a_{vt}} \frac{b_{1_{vt}}}{b_{2_{vt}}}$$

v. Stick force and stick force gradient

$$F_{s_r} = -G_r \frac{1}{2} \rho V^2 \eta_{vt} S_r \overline{c}_r \left[\left(b_{1_r} + b_{2_r} \frac{C_{n_\beta}}{C_{n_{\delta_r}}} \right) \beta - b_1 \sigma \right]$$

$$\frac{dF_{s_r}}{d\beta} = - \frac{G\frac{1}{2}\rho V^2 \eta_{vt} S_r \bar{c}_r b_{r_r}}{C_{n_{\delta_r}}} \hat{C}_{n_{\beta}}$$

b. Roll stability parameter (vertical tail contribution only)

$$C_{l_{\beta}} = a_{\nu t} \eta_{\nu t} V_{\nu t} \left(1 - \frac{\partial \sigma}{\partial \beta} \right) \frac{z_{\nu t}}{l_{\nu t}} < 0 \text{ for stability}$$

8. General lateral-directional steady state equations

$$\begin{bmatrix} C_{Y_{\beta}} & C_{Y_{\delta_{a}}} & C_{Y_{\delta_{r}}} & C_{Y_{p}} & C_{Y_{r}} & C_{w} \\ C_{l_{\beta}} & C_{l_{\delta_{a}}} & C_{l_{\delta_{r}}} & C_{l_{p}} & C_{l_{r}} & 0 \\ C_{n_{\beta}} & C_{n_{\delta_{a}}} & C_{n_{\delta_{r}}} & C_{n_{p}} & C_{n_{r}} & 0 \end{bmatrix} \begin{bmatrix} \beta \\ \delta_{a} \\ \delta_{r} \\ \hat{p} \\ \hat{r} \\ \varphi \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ -C_{n_{T}} \end{bmatrix}$$

Pick a set of three variables and solve for the remaining three. For a steady turn

$$\hat{p} = -\frac{\omega b}{2 V} \sin \theta$$
$$\hat{r} = \frac{\omega b}{2 V} \cos \phi \cos \theta$$

9. Some aerodynamic estimation formulas

a. Lift curve slope

$$a_{wing tail} = \frac{2 \pi AR}{2 + \sqrt{\frac{AR^2 (1 - M^2)}{k^2} \left(1 + \frac{\tan^2 \Lambda_{c/2}}{(1 - M^2)}\right) + 4}}$$

where $k = \frac{c_{l_{\alpha}}}{2\pi}$, actual 2-D lift-curve slope / theoretical-flat-plate 2-D lift-curve slope

b. Downwash parameter

$$\frac{\partial \epsilon}{\partial \alpha} = 4.44 \left[K_a K_\lambda K_H \left(\cos \Lambda_{\frac{c}{4}} \right)^{\frac{1}{2}} \right]^{1.19}$$

where

$$K_{A} = \frac{1}{AR} - \frac{1}{1 + AR^{1.7}}$$

$$K_{\lambda} = \frac{10 - 3\lambda}{7}$$

$$K_{H} = \frac{1 - \left|\frac{h_{H}}{b}\right|}{\sqrt[3]{\frac{2\bar{l}_{ht}}{b}}} \quad \text{where} \quad \bar{l}_{ht} = (h_{ht} - h_{n_{wb}})\bar{c}$$

11. Basic Equations of Motion

 $\overline{V}^{b} = u\hat{i}^{b} + v\hat{j}^{b} + w\hat{k}^{b}$ is the velocity vector represented in body fixed coordinates. $\overline{\omega} = p\hat{i}^{b} + q\hat{j}^{b} + r\hat{k}^{b}$ is the angular rate vector represented in body fixed coordinates. Then the differential equations of motion are:

a. Force Equations

$$F_{x} = m(\dot{u} + qw - rv)$$

$$F_{y} = m(\dot{v} + ru - pw)$$

$$F_{z} = m(\dot{w} + pv - qu)$$

b. Moment Equations

$$L = I_{x}\dot{p} + (I_{z} - I_{y})qr - I_{xz}(pq + \dot{r})$$

$$M = I_{y}\dot{q} + (I_{x} - I_{z})pr + I_{xz}(p^{2} - r^{2})$$

$$N = I_{z}\dot{r} + (I_{y} - I_{x})pq + I_{xz}(rq - \dot{p})$$

c. Kinematic Equations

$$\dot{\Phi} = p + \tan \theta (q \sin \phi + r \cos \phi)$$
$$\dot{\theta} = q \cos \phi - r \sin \phi$$
$$\psi = \sec \theta (q \sin \phi + r \cos \phi)$$

2. Forces - Aerodynamic, Gravitational, Thrust

a. Aerodynamic (for body fixed stability axes) and Thrust

$$Fx_T + Fx_A = T_x - Drag$$
 $Fy_T + Fy_A = T_y + Y Fz_T + Fz_A = T_z - Lift$

b. Gravitational (for body fixed (any) axes)

$$Fx_g = -mg \sin \theta$$
 $Fy_g = mg \cos \theta \sin \phi$ $Fz_g = mg \cos \theta \cos \phi$